

1.

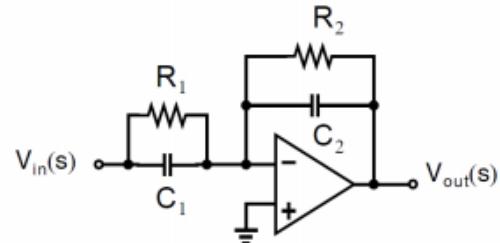
$$V_{out}(s) = \frac{-1}{sC_2} \left[(1/R_1 + sC_1)V_{in}(s) + V_{out}(s)/R_2 \right]$$

$$\frac{V_{out}(s)}{V_{in}(s)} = -\frac{R_2}{R_1} \frac{1 + R_1 C_1 s}{1 + R_2 C_2 s}$$

The opamp has a frequency response

$$A(s) = \frac{A_0}{1 + \frac{sA_0}{\omega_{la}}}$$

Denoting the negative opamp input terminal voltage, V_x , we may write a nodal equation there as follows:



$$\frac{V_{in} - V_x}{R_1 \parallel 1/sC_1} = \frac{V_x - V_{out}}{R_2 \parallel 1/sC_2}$$

Substituting in $V_{out} = -A(s)V_x \Rightarrow V_x = -V_{out}/A(s)$:

$$\frac{V_{in} + V_{out}/A(s)}{R_1 \parallel 1/sC_1} = \frac{-V_{out}/A(s) - V_{out}}{R_2 \parallel 1/sC_2}$$

Using the expression for $A(s)$ above and rearranging yields:

$$\frac{V_{out}(s)}{V_{in}(s)} = -\frac{R_2}{R_1} \frac{A_0}{1 + A_0} \frac{1 + R_1 C_1 s}{1 + R_2 C_2 s} \frac{1}{1 + s/\omega_{la}}$$

2. KCL at C1: $-gm1.V1 - gm2.V2 + gm4.Vo = sC1.V2$

KCL at C2: $-gm3.V2 = sC2.Vo$

$$H_o(s) = Vo/V1 = gm1.gm3 / (s^2.C1.C2 + s.gm2.C2 + gm3.gm4)$$

$$H1(s) = V2/V1 = (-sC2 / gm3) H_o(s) = -sC2.gm1 / (s^2.C1.C2 + s.gm2.C2 + gm3.gm4)$$

3. By interreciprocity, $V_o = - \sum I'_k V_k$. Using Bashkow's method, we assume $I'_1 = 1 \text{ A}$, and also to simplify the calculations, $R = 1$ (this doesn't change the voltage gain). Then $V_a' = 2$, $I_2' = 2$, $I_b' = 3$, $V_b' = 5$, $I_3' = 5$, $I_c' = 8$, $V_c' = 13$, $I_4' = 13$, $I_d' = 21$.

Hence, the scale factor is $-1/21$, and $V_o = (1/21) [1x1 + 2x1 + 5x2 + 13x2] = 39/21 \sim 1.857 \text{ V}$.

